

1 compounds identification using GC/MS showed that the combination between wall material
2
3 and inlet air temperature was effective to retain phenol as one of liquid smoke bioactive
4
5 compounds. Microcapsules morphology analysis showed that the average diameter of
6
7 microcapsules was 4.28 μm and had nearly spherical shape, little shriveled, and without
8
9 agglomeration with low levels of damage.

10
11 **Keywords:** Refined liquid smoke, broken rice, maltodextrin, spray drying, liquid smoke
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13 microcapsules.

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1 **Nomenclature**

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3 LS : Liquid smoke

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5 IR : Indica Rice

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7 DE : Dextrose Equivalent

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9 FF : Fehling Factor

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11 TSS : Total Soluble Solid

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13 db : Dry basis

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15 wb : Wet basis

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1 **1. Introduction**

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3 Liquid smoke (LS) is condensate obtained from the condensation of wood smoke produced
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5 by smoldering wood chips or sawdust under limited oxygen and constituent pyrolysis of
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7 wood such as cellulose, hemicellulose, and lignin (Panagan and Nirwana, 2009; Darmadji,
8
9 1996). Refined LS contains active compounds such as phenols, carbonyls and organic acids
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11 (Girard, 1992; Maga, 1998; Bratzler et al., 1969), so it can be used as a safe alternative food
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13 preservative without carcinogenic (Budijanto et al., 2008) and mutagenic materials
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15 (Kažimírová and Jablonická, 1994), as well as anti-bacterial and fungicide materials in
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17 certain doses (Pszczola, 1995; Dwiyitno and Rudi, 2006). Moreover, LS can act as an
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19 antioxidant (Saloko et al., 2014). However, LS has a disadvantage that is easily damaged
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21 during storage and sensitive to environmental factors (light, temperature, oxygen), so the
22
23 technology that can protect the active compound is needed, one of which is encapsulation
24
25 technique.

26
27 Encapsulation is a process of coating a core material that can be either very small liquid/gas
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29 particles with an encapsulant agent so that the core particles have physical and chemical
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31 properties as desired (Kim et al., 1996). Encapsulation provides protection of the LS
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33 bioactive compounds in an encapsulan at a very small size and potential to change the shape
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35 of the liquid to the flour that is stable, so easily applied to the food. In addition,
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37 encapsulation can change the liquid product into a powder, making it easier to handle.

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39 The successful of encapsulation process is influenced by the selection of technology and
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41 materials as encapsulant agent. Encapsulation by spray drying technique is economical,
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43 safe, and applicable (Chan, 2011), therefore it is commonly used in the production of
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1 microcapsules. In the spray drying process, quality and efficiency of the final product is
2
3 influenced by the operating conditions including inlet air temperature and feed
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5 concentration (wall material) (Amerie and Maa, 2006; Chegini and Ghobadian, 2005; Goula
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7 and Adamopoulos, 2008; Tonon et al., 2008; Caliskan and Dirim, 2013).

8
9 The the appropriate of encapsulant agent will improve the efficiency of micro-encapsulation
10
11 by protecting the active compounds from heat. However, if the amount of encapsulant agent
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13 used is too high can cause delution effect, thus causing a decrease in the chemical content of
14
15 the material (Şahin-Nadeem et al., 2013; Şahin-Nadeem et al., 2011). Thies (2001)
16
17 explained that the amount of coating material that is commonly used for commercial
18
19 microcapsules obtained by spray drying technique is 20–30 %.

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21 Inlet air temperature also affects the resulted microcapsules. Inlet air temperature that is too
22
23 low can cause low evaporation rate causing formation microcapsules with high density
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25 membrane, high moisture content, poor fluidity, and prone to agglomerate. However, if the
26
27 inlet temperature is high, it can lead to excessive evaporation and lead to cracking of the
28
29 membrane that triggers premature release formation and a decrease in the amount of
30
31 encapsulated or core materials (Zakarian and King, 1982 dalam Gharsallaoui et al., 2007).

32
33 Maltodextrin is a common ingredient used as a encapsulant/coting agents on
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35 microencapsulation process by spray drying technique to increase the capacity of the drying
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37 process and lowering the stickiness and agglomeration problems during storage, thus a
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39 stable product can be obtained (Anwar and Kunz, 201; Hogan et al., 2001; Shu et al., 2006;
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41 Teixeira et al., 2004; Bylaite' et al., 2001; Shaikh et al., 2006). Commercial maltodextrin can
42
43 be obtained from three plant sources, such as corn starch, potato, and rice. Indonesia is the
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1 world's third-largest rice producer after China and India. According to FAOSTAT 2014,
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3 Indonesian rice production in 2012 reached 69,045,141 mT. In the rice milling process,
4
5 about 15 % broken rice is resulted (Bhullar and Bhullar, 2013). Rice (*Oryza sativa* L.) is
6
7 potential source with 90 % starch content. On the other hand, broken rice is abundant and
8
9 cheap by-product of rice processing in Indonesia, thus make it highly potential to be used to
10
11 produce maltodextrin.

12
13 Based on those descriptions, the research on the broken rice utilization as material for
14
15 refined LS encapsulation was done. The appropriate of spray drying operating conditions in
16
17 this case the inlet temperature and feed concentration (amount of maltodextrin), led to
18
19 produce microcapsules with good quality and efficiency.

20 21 **2. Materials and methods**

22 23 2.1. Materials

24
25 LS grade I (food grade) was obtained from PT. Tropica Nucifera Industri with pH 2.5 and
26
27 phenol total 18.83 % (db). Enzyme α -amylase from *B. licheniformis* (Sigma Chemical Co,
28
29 St. Louis, USA), chitosan obtained from PT. Biotech Surindo-Cirebon with MW 2183778,
30
31 DD 87 %, viscosity 44.4 cP, moisture content 7.65 %, and ash content 1.04 %. Broken rice
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33 IR 64 obtained from local rice mill in Somberembe Hamlet, Village Slomartari, Kalasan
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35 district, Sleman regency, Yogyakarta in February 2014. Other chemicals were Na_2CO_3 ,
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37 CaCl_2 , folinciocalteau, pure phenol, aquadest, HCl, NaOH, helium and whatman no. 41 and
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39 no. 1 filter paper.

40 41 2.2. Starch broken rice extraction

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43 Broken rice was processed by wet-milled method as described by Hoe et al. (2013) with
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1 some modifications. Broken rice was soaked in water for 4 hours, then ground. Processing
2
3 of broken rice into flour was made in a traditional market in Yogyakarta, then dried with a
4
5 cabinet dryer at 50 °C for 24 h to reach moisture content of ~14 %, then sieved with an 80
6
7 mesh sieve.

8
9 Starch was extracted by protein alkaline protein extraction method as described by Lim et
10
11 al. (1991) with modification. 100 g rice flour soaked in 500 mL of 0.15 M NaOH for 24
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13 hours. The slurry was then stirred for 30 minutes at 400 rpm and centrifuged at 2226 g for
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15 20 min. The formed sediment was then dissolved in 500 mL of water and then filtered. The
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17 solution was then neutralized with 3 M HCl and centrifuged at 2226 g for 15 min. The
18
19 formed sediment was washed 3 times with water by centrifugation at 2226 g for 15 min,
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21 where dark tailing on top layer was scraped while washed. The obtained starch was dried at
22
23 50 °C for 24 h to reach moisture content of ~8.3 %, then ground and sieved with a 60 mesh
24
25 sieve.

26 27 2.3. Broken rice starch maltodextrin production

28
29 100 g broken rice starch was dissolved in 400 mL of distilled water and 40 ppm CaCl₂ was
30
31 added as a catalyst, then the pH was adjusted to 6 using 0.1 N HCl solution and then added
32
33 0.005 mL α -amylase. Hydrolysis was performed at 87±1 °C, for 15 with agitation. Enzyme
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35 was inactivated by cooling down to 27 °C, and pH was adjusted to 3±0.5 using 0.1 N HCl.
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37 Suspension was incubated for 30 minutes then added 0.1 N NaOH to reach pH ± 6. The
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39 obtained dark solution was centrifuged for 30 minutes at 2226 g. The upper clear layer was
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41 then poured slowly on whatman no. 41 filter paper that had been installed on the vacuum
42
43 pump. The clear solution was then dried at 50 °C for 3 days to reach moisture content of
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1 ~3.9 %, then ground and sieved with a 60 mesh sieve to obtain maltodextrin.

2 2.4. Microparticle preparation

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4
5 Wall material used was maltodextrin obtained from previous process at total soluble solid
6
7 (TSS) of 20%, 25% and 30%, each combined with 1% w/w chitosan. Based on research
8
9 orientation, the amount of maltodextrin and chitosan added in refined LS solution to reach
10
11 TSS 20, 25, and 30 % can be seen in Table 1. Wall material was dissolved into 100 mL
12
13 refined LS, stirred using magnetic stirrer (400 rpm, 30 minutes, room temperature), and
14
15 homogenized using homogenizer (Ultraturrax T50 Basic IKA Werke, Germany) at 4000
16
17 rpm for 2 minutes. Mixture was then filtered by paper filter to separate insoluble precipitate.
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19 Microparticle liquid was stored in cool room to prevent oxydation.

20 2.5. Spray drying

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23 Microcapsule of refined LS was prepared using spray drying method (Lab Plant Sd 05,
24
25 UK). Inlet air temperature to dry liquid smoke microparticle were 120, 130, and 140 °C,
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27 with flow rate of 5 mL/minute, nozzle atomizer pressure of 1 bar, and stable drying air
28
29 volume. Obtained microcapsule powder was placed into air-tight plastic container equipped
30
31 with silica gel before stored in low humidity cool room for further analysis.

32 2.6. Analysis methods

33 2.6.1. Dextrose equivalent

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36 DE of broken rice starch maltodextrin was conducted according Shi *et al.* (2000).

37 a. Fehling Factor Value

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41 2.5 g of glucose was dissolved in 1000 mL of distilled water. 15 mL solution was taken and
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43 added each 5 mL Fehling's solution A and B. Mixture was then boiled and titrated
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1 immediately with glucose solution until the blue color completely disappear and changed to
2
3 be reddish brown. The amount of titrant was then recorded, and Fehling Factor calculated
4
5 by :

$$6 \quad FF \times \frac{\text{Titant (mL)} \times \text{glucose weight (g)}}{1000} \quad (1)$$

10 a. DE Value Determination

11
12 Maltodextrin 10 g was dissolved in 200 mL of distilled water, then poured into the burette.
13
14 50 mL of distilled water was added each 5 mL of Fehling's solution A and B and 15 mL of
15
16 glucose solution. Mixture was then boiled and titrated immediately with maltodextrin
17
18 solution until the blue color completely disappear and changed to be reddish brown. The
19
20 amount of titrant was then recorded, and DE calculated by:

$$21 \quad DE = FF \times \frac{100}{\text{Maltodextrin solution concentration (g/mL) x titrant (mL)}} \quad (2)$$

25 2.6.2. Moisture Content

26
27 Moisture content of microcapsules and maltodextrin was measured using moisture tester
28
29 (Ohaus MB 35 halogen, England), due to highly hygroscopic properties of sample by drying
30
31 as much as 500 mg sample at 150 °C for about 2 minutes till constant weight. Moisture
32
33 content of refined LS was determined by toluene distillation method according to AOAC,
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35 1970.

37 2.6.3. Ash content

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39 Ash content of broken rice starch maltodextrin was conducted according to AOAC Official
40
41 Method 923.03 (AOAC, 1990).

1 2.6.4. Solubility

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3 Solubility was analyzed according to Loksuwan (2006) method with major modification.
4
5 0.5 g sample was mixed with 50 ml of distilled water using a magnetic stirrer at room
6
7 temperature for 30 minutes then filtered using whatman no.1 filter paper which had
8
9 previously been dried to constant weight. Filter paper was then dried at 60 °C to constant
10
11 weigh, then the solubility calculated by its weight. Equation was as follows:

$$12 \text{ Solubility (\%)} = \frac{\text{Sample (g)} - \text{Retante (g)}}{\text{Sample (g)}} \times 100 \quad (3)$$

15 2.6.5. Total soluble solid

16
17 Total Soluble Solid was measured according to AOAC (2005), by dropping sample solution
18
19 on hand refractometer. TSS was calculated based on the percentage of dissolved solids in
20
21 solution refined LS microparticle.

23 2.6.6. Microcapsule yield

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25 Yield was measured by comparing microcapsule weight with amount of total soluble
26
27 solid/TSS, where TSS value was previously measured based on liquid smoke weight.

29 2.6.7. Phenol total

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31 Phenol total was analyzed using Senter et al. (1989) method with slight modification. For
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33 refined LS, as much as 1 g of refined LS was weighted and dissolved into 100 mL distilled
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35 water, then 10 mL taken from it to dissolved again into 100 mL. For refined LS
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37 microcapsules, as much as 0.5 g was dissolved into 50 mL, then 5 mL taken from it to
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39 dissolved in the 100 mL flask with distilled water (dilution factor = 1000x). 1 mL from each
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41 final solution was put into tube, added with 5 mL Na₂CO₃ 2 % alkali, incubated for 10
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43 minutes at room temperature, then added with 0.5 mL folin ciocalteau reagen, and shaken
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1 using vortex before 30 minutes incubation in room temperature. Absorbance was measured
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3 at 750 nm. Phenol total of refined LS and refined LS microcapsules was calculated using
4
5 standard curve equation previously obtained.

6 2.6.8. Microencapsulation efficiency (ME)

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8 Efficiency of refined LS microcapsules was calculated based on phenolic content of refined
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10 LS, reflected amount of capsulated phenolic compound. Calculation was made using
11
12 Cvitanović et al. (2011) equation, which comparing phenol total contained in microcapsule
13
14 and in initial refined LS (before encapsulation). Phenol weight in microcapsule (% db) was
15
16 multiplied with the weight of microcapsule obtained. Equation was as follows:
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$$18 \quad \text{ME (\%)} = \frac{\text{Phenol in microcapsul (g)}}{\text{Phenol in microparticle solution (\% db)}} \times 100 \quad (4)$$

$$19 \quad \text{Phenol in microparticle solution (\% db)} = \frac{\text{Phenol in LS (\% db)} \times \text{LS Weight (g)}}{\text{Total soluble solid (g)}} \times 100 \quad (5)$$

$$20 \quad \text{Phenol in micro- capsules (g)} = \text{Phenol total microcapsules (\% db)} \times \text{Microcapsule weight (g)} \quad (6)$$

21 2.6.9. Phenol release

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23 Phenol Release was conducted according to Lokuwan (2006) solubility method with major
24
25 modification. Refined LS microcapsules 1 % (w / v) in distilled water was stirred
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27 sustainably at 400 rpm. Furthermore, 5 mL solution was taken at minute 1st, 3nd, 6nd, 10nd,
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29 20nd, 30nd and 40nd then dissolved in the 100 mL flask with distilled water for phenol total
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31 analysis measured according to Senter et al. (1989) method.
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41 2.6.10. Microcapsule morphology

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43 Appearance and shape (morphology) of refined LS microcapsules was observed using
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1 Scanning Electron Microscopy (SEM) according to Cerdeira et al. (2005) method, by
2
3 placing microcapsule samples on aluminum plate using adhesives, coated with thin layer of
4
5 gold before observation using SEM instrument at 5 kV voltage and 5000 times
6
7 magnification.

9 2.6.11. Volatile compound identification

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11 Identification of volatile compounds in microparticle and microcapsules was referred to the
12
13 method by Chin et al. (2010) with modification. Refined LS microparticle was directly
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15 injected into GC-MS, while refined LS microcapsules need to be prepared before injection.
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17 As much as 0.25 g of microcapsules were suspended into 10 mL deionized water, shaken
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19 using vortex for 30 minutes, and kept inside sealed conical tube prior to GC-MS injection.
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21 Analysis conducted using GCMS-QP2010S Shimadzu. Splitl injection mode with injection
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23 port temperature of 250°C was used. Column was AGILENT HP 5MS with anlength x
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25 internal diameter x thickness of the film = 30 m x 0.25 mm x 0.25 µm. Oven temperature
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27 was run gradiently with the settings set to 60°C held 1 min, then raised to 280 °C at a rate of
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29 5°C/min and held for 21 min. Carrier gas was helium at a rate of 0.51 mL/min. Detector was
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31 MS (Mass Spectrometer) with ionization energy 70 eV scan mass range (m/z) 28–600 with
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33 a 250°C detector temperature.

35 2.7. Experimental design

36
37 Completely randomized experiment design was used in this study with two factorials (inlet
38
39 air temperature and concentration of wall material), where TSS consisted of 20, 25, and 30
40
41 % and inlet air temperature consisted of 120, 130 and 140 °C. The differences between the
42
43 mean values of multiple groups were analyzed by one-way analysis of variance (ANOVA)
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1 with Duncan's multiple methods range tests. ANOVA data with a $p < 0.05$ was classified as
2 statistically significant. SPSS 17.0 statistics and Microsoft Excel 2010 program were used.

3 **3. Result and discussion**

4 5 6 7 3.1. Characterization of maltodextrin broken rice starch

8 Maltodextrin broken rice starch obtained showed that maltodextrin had characteristics as
9 standard requirements of commercial maltodextrin (Table 2), such as white to yellowish
10 powder or concentrate solution, high solubility, 6 % of maximum water content, pH 4.5–
11 6.5, 0.6 % of maximum ash content, and DE < 20 (Akhilesh et al., 2012; Wang and Wang,
12 2000; Storz and Steffens, 2004). According to the USA Food and Drug Administration, the
13 maltodextrins are defined a starch hydrolyzate product that is not sweet with DE less than
14 20 and they are classified as ingredients generally recognized as safe (GRAS) (Marchal et
15 al., 1999).
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25 One of the determinants of the maltodextrins quality is their solubility in water. Good
26 quality maltodextrin has a high solubility index. The result showed that (Table 2) broken
27 rice starch maltodextrin solubility produced was quite high. Wang and Wang (2000),
28 observed that maltodextrin derived from rice starch had short chain. The high solubility of
29 maltodextrin produced allegedly caused by its short linear chain of maltodextrin rice starch
30 and led to lower molecular weight, thus solubility became high. This is supported with
31 Yusraini et al., (2013), who stated that the longer linear chain caused higher molecular
32 weight, so poorly soluble in water.
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41 3.2. Microcapsule yield

42 One of the factors that can affect the amount of yield produced on microencapsulation using
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1 spray drying technique is the amount of wall material added. The low percentage yield
2
3 produced can be caused by two possibilities. The first, the least concentration of the added
4
5 wall materials will cause evaporation of active compounds due to lack of materials that can
6
7 bind and retain the active compounds from high temperature contact that can degrade their
8
9 concentration during drying process. The second possibility is the increasing concentration
10
11 of the wall materials may cause an increase in the viscosity of the microparticle solution. If
12
13 the viscosity of microparticle solution is high, it will lead to produce microcapsules with
14
15 high moisture content due to temperature equilibrium during the drying process faster, thus
16
17 there will be attachment a large number of microcapsules produced in dryer chamber
18
19 (Tonon et al., 2008; Krishnaiah et al., 2012).

20
21 The recent study showed that the increase in yield positively correlated with increasing wall
22
23 material concentrations used (Table 3) (TPT 30 %), but showed no significant increase ($p >$
24
25 0.05), except in the 140 °C inlet air temperature ($p < 0.05$) in which the more wall materials
26
27 used, the yield of produced percentage will be higher. This can be caused by an increase in
28
29 the total solids in microparticle solution (Şahin-Nadeem et al., 2011; Şahin-Nadeem 2013).

30 31 3.3. Microcapsule moisture content

32
33 Moisture content of refined LS microcapsules (Table 3) was decreased with the increase of
34
35 TSS concentration and spray drying inlet temperature, with lowest value obtained at 30 and
36
37 20 %TSS and all inlet air temperature ($p < 0.05$). The higher inlet air temperature causes the
38
39 increase of water mass transfer through surface evaporation resulting microcapsules with
40
41 low moisture content (Krishnaiah *et al.*, 2012). This result was consistent with study by
42
43 Saloko *et al.* (2012) and Şahin-Nadeem *et al.* (2013).

44

1 Lower moisture content was also obtained by increasing wall material concentrations. The
2
3 addition of maltodextrin on solution prior to drying process will increase TSS and lower
4
5 moisture content of solution that will be evaporated during the drying process, thus lead to
6
7 the decrease of water content in the final product (microcapsules). This indicates that the
8
9 addition of maltodextrin concentrations is able to lower water content in the produced
10
11 microcapsules (Krishnaiah et al., 2012). This result is in accordance with study by Şahin-
12
13 Nadeem et al. (2011) which encapsulated mountain tea (*Sideritis stricta*) extract.

14 15 3.4. Microcapsule solubility

16
17 The use of inlet air temperature on the same TSS showed no significant difference
18
19 ($p > 0.05$) (Table 3), except in TSS 30 % with 140 °C inlet air temperature. High inlet air
20
21 temperature can lead to the possibility to form hard surface layer microcapsules thus
22
23 lowering microcapsules wettability and reduce the solubility (Goula and Adamopoulos,
24
25 2004). Instead, Low inlet air temperature causes microcapsule water content high allowing
26
27 agglomeration that can accelerate the reconstitution of the microcapsules in the water. The
28
29 same results have also been reported by Şahin-Nadeem et al. (2013).

30
31 Another possibility which can lead to decrease levels of solubility in TSS 30 % is the
32
33 presence of amylose retrogradation on maltodextrin used. Unhydrolyzed amylose will form
34
35 an opaque gel and also affects dissoluble microcapsule particles (Yusraini et al., 2013).
36
37 Wang and Wang (2000) stated that the maximum concentration of maltodextrin is about 30
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39 %.

40 41 3.5. Phenol total

42
43 In Table 3, phenol total of refined LS microcapsules decrease in concomitant with the
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1 increase of TSS, due to higher concentration of solid able to diminish phenol content of
2
3 final products (dilution effect). This result is in agreement with study by (Caliskan and
4
5 Dirim, 2013; Şahin-Nadeem et al., 2013; Şahin-Nadeem et al., 2011).
6
7 Higher inlet air temperature (140 °C with 20 and 25 % TSS) lead to increase phenol total of
8
9 microcapsules ($p < 0.05$). Higher inlet air temperature causes low water content of the
10
11 microcapsules, thus phenol concentrated resulting a higher phenol total consequently.
12
13 However, that was not occurred at 30 % TSS, which was caused by the contribution of
14
15 higher total solids (dilution effect) as mentioned before. Şahin-Nadeem et al. (2011)
16
17 encapsulated mountain tea extract and reported that there was an increase in phenol totals in
18
19 the sample by 4 % with the increase in inlet temperature of 145–155 °C, but the increase in
20
21 inlet temperatures up to 165 °C resulted in a slight decrease in phenol totals. Şahin-Nadeem
22
23 et al. (2013) encapsulated sage instant and reported an increase in phenol totals at 145–165
24
25 °C inlet temperature, but the increase is not significant.Çam et al. (2013) encapsulated
26
27 phenolicpomegranate peel by 4 types of maltodextrin and showed an increase in phenol
28
29 content at 130–160 °Cinlet temperature, but did not show a significant increase.

30 3.6. Phenol release

31
32 The recent study (Fig. 1) showed that at inlet air temperatur 120 and 130 °C with 20, 25 and
33
34 30 % TSS, the whole phenol in the microcapsules released at minute 10th, 10th, and 3th,
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36 while at inlet air temperatur 140 °C with 20, 25 and 30 % TSS, the whole phenol in the
37
38 microcapsules released at minute 20th, 20th, and 30th. The increase of wall materials used
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40 caused the phenol released faster. In addition to be caused by using more maltodextrin
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42 (Loksuwan, 2006) that caused higher solubility of microcapsule, thus affected the
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1 accelerated released of phenolic compounds, another cause was the increasing amount of
2
3 wall materials used caused lower phenol total content (Table 3), so that tme release for
4
5 releasing phenol in microcapsules entirely became shorter.

6
7 Inlet air temperature also affected phenol release of microcapsules. Seen clearly in Fig.1, in
8
9 the higher inlet air temperature, phenol content of the microcapsules will be greater and it
10
11 affectes the increasing duration release of phenol compounds. Another thing that plays a
12
13 role in the phenol release is the ability of chitosan added to bind phenolic compounds (Popa
14
15 et al., 2000). At 140 °C inlet air temperature with 30 % TSS, microcapsules showed the
16
17 ability to retard phenol release up to 30 minutes. Hsieh et al., (2006) observed that, by
18
19 increasing chitosan concentration on microencapsulation of citronella.oil, it was able to
20
21 increase its time release. Saloko et al. (2014) reported that, combination of maltodextrin-
22
23 chitosan as material agent in encapsulated LS showed a significant difference in improving
24
25 phenol total content compared with LS without chitosan.

26 27 3.7. Microencapsulation efficiency (phenol)

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29 Interestingly, microcapsules with 25 % TSS showed a significant increase in
30
31 microencapsulation efficiency compared with 20 % TSS ($p < 0.05$) (Table 3), however at 30
32
33 % was not so. This suggested that the use of higher wall materials did not give a significant
34
35 effect on improving of microencapsulating efficiency. Microencapsulation efficiency can be
36
37 increased by increasing wall solution solids concentration which can be related to the effect
38
39 of wall solids concentration on the formation of surface core prior to the formation of crust
40
41 around the drying droplets (Young et al., 1993 in Gharsallaoui et al., 2007). Similar results
42
43 have also been investigated by Caliskan and Dirim (2013) which encapsulated sumac
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1 extract using maltodextrin and concluded that the highest efficiency was obtained from the
2
3 extract containing 25 % TSS. However, using higher TSS (30 %) can reduce efficiency due
4
5 to the dilution effect as described previously. Çam et al. (2013) conducted a phenolic
6
7 encapsulation pomegranate peel with 4 types of maltodextrin and showed that the increase
8
9 in the ratio between maltodextrin with phenolic encapsulated had a degradation effect on
10
11 microencapsulation efficiency.

12 Inlet air temperature significantly influence the resulting microencapsulation efficiency.
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14 Inlet air temperature related directly to the drying rate and moisture content of
15
16 microcapsules. When the air inlet temperature is low, the low evaporation rate causes the
17
18 formation of microcapsules with high density membranes, high water content, poor fluidity,
19
20 and easiness of agglomeration. However, a high air inlet temperature causes an excessive
21
22 evaporation and results in cracks in the membrane inducing subsequent premature release
23
24 and a degradation of encapsulated ingredient or also a loss of volatiles (Gharsallaoui et al.,
25
26 2007). Çam et al. (2013), reported that at 160 °C inlet air temperature showed that yield,
27
28 efficiency, and phenol total of phenolic pomegranate peel microcapsules was higher than at
29
30 130, 140, and 150 °C. However, at inlet temperatures above 160 °C showed no significant
31
32 improving.

33 3.8. Microcapsule morphology

34
35 Analysis was conducted on microcapsule prepared using TSS 25 % and inlet air temperature
36
37 of 140 °C as best treatment based on highest phenol efficiency. Selected image from the
38
39 SEM microstructure analysis of the refined LS microcapsule is illustrated in Fig. 2. The
40
41 SEM result showed that microcapsules had nearly spherical shape, little shriveled, and
42
43
44

1 without agglomeration with low levels of damage.
2
3 Microcapsule morphology of the resulted microcapsules of various microencapsulation of
4
5 active compounds by using maltodextrin as a single wall material by spray drying technique
6
7 showed shrinkages on the surface, shriveled, and even had an irregular shape(Tonon et al.,
8
9 2008; Şahin-Nadeem et al., 2011; Şahin-Nadeem et al., 2013; Caliskan and Dirim, 2013;
10
11 Saloko et al., 2012).When compared with the results obtained (Fig. 2), it is proved that
12
13 using combination of maltodextrin-chitosan as material agents gives better result. Chitosan
14
15 as biofilms can provide a stable layer structure and act as a good barrier, thus able to protect
16
17 the coated bioactive compounds (Honarkar and Barikani, 2009).

18 19 3.9. Volatile compound identification

20
21 Analysis was conducted on microparticle solution and microcapsule prepared using TSS 25
22
23 % and inlet air temperature of 140 °C as best treatment based on highest phenol efficiency.
24
25 Fifteen compounds were identified as described in Table 4. There are two compounds with
26
27 the highest concentration, i.e. acetic acid and phenol. This proves that LS contains
28
29 components phenol and organic acids in high quantities. Maga (1998) has observed that
30
31 liquid smoke from wood material composed of 11–92 % water, 0.2–2.9 % phenolic, 2.8–4.5
32
33 % organic acid, and 4.6–2.6 % carbonyl. Bratzler et al., (1969), stated that the main
34
35 component of wood smoke condensate, consisting of carbonyl (24.6 %), carboxylic acid
36
37 (39.9 %), and phenolic compounds (15.7 %).

38
39 After micro-encapsulated refined LS using broken rice starch maltodextrin using 25 % TSS
40
41 + chitosan 1 % and 140 °C inlet air temperature, 7 volatile compounds were identified,
42
43 wherein the solution of microparticle previously identified 13 volatile compounds. This
44

1 suggests that during the spray drying process involving high heat transfer can cause the loss
2 of some volatile compounds (Nesterenko et al., 2013). In addition, high heat also causes the
3 formation of a new compound in microcapsules. However, a phenolic compound that is the
4 main bioactive component of liquid smoke can be protected with the use of materials which
5 act as a protective coating. (Young et al., 1993 in Gharsallaoui et al., 2007). This proves that
6 maltodektrin as wall material agent can prevent the degradation of the active ingredient
7 (phenol) microcapsules produced (Gustavo and Canovas, 1999).
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14 **4. Conclusion**

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17 Combination of 25 % broken rice starch maltodextrin and 1 % chitosan (w/w) as wall
18 materials and the applied 140 °C air inlet temperature showed good ability to coated refined
19 LS compared to others based on analysis, phenol total, microencapsulation efficiency, yield
20 and phenol release and had high solubility. Microcapsules morphology analysis showed that
21 microcapsules had nearly spherical shape, little shriveled, and without agglomeration with
22 low levels of damage. Microcapsules average diameter was 0.24 µm.
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32

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